

VOL'SKIY, Viktor Votslavovich; GLINKIN, Anatoliy Nikolayevich; LAVRENT'YEVA,
Ye.V., redaktor; NOGINA, M.I., tekhnicheskii redaktor.

[Brazil] Braziliia, Moskva, Gos. izd-vo geogr. lit-ry. 1956. 87 p.
(Brazil--Geography) (MIRA 9:5)

GLINKIN, I.

State Bank's business and credit plan for 1967
60 p. 1967.

1. Upravlyayushchiy i obshchestvennyy sektor
oblasti.

Upravlyayushchiy i obshchestvennyy sektor

GLINKIN, M. I.

U.S./Medicine - Literature
Sanitation

Aug 49

"Sanitation Service in the Days of the Patriotic War: Vol. II, Gunshot Aneurisms,"
Medgiz, 1948, 1 p

"Khirurgiya" No 6

Volume contains 14 works of collaborators in two specialized hospitals of the Ural
Mil Dist on clinical problems and treatment of traumatic aneurisms. Contributors
are: L. M. Ratner, L. M. Protalinskaya, M. K. Glinkin, I. D. Komabel'nikov, and
A. I. Bogatov.

PA 1/50367

GLINKIN, N.A., kand.tekhn.nauk

Axonometric templates. Izv.vys.ucheb.zav.; mashinostroyeniye, no. 11, 1960, p. 11-12.
'60. (DIA 10-50)

1. Moskovskiy aviatsionnyy institut.
(Drawing instruments)

GLINKIN, N. M.; YERUKHMANOV, M. I.; STEIN, G. S.;

Spravochnik Mastera Metallobrabyvayushchego Tsekh, published by Mospromstroi,
Moscow, 1960

~~xxxx~~ Sum #116

YEGOROV, M.Ye., zasluzhennyy deyatel' nauki i tekhniki, doktor tekhn.
nauk, prof.; GLINKIN, N.M., dotsent, red.; KUNIN, P.A., red.;
CHERNOVA, Z.I., tekhn.red.; SOKOLOVA, T.F., tekhn.red.

[Fundamentals of designing machinery plants] Osnovy proektiro-
vaniia mashinostroitel'nykh zavodov. Izd.5., perer. Moskva,
Gos.nauchno-tekhn.izd-vo mashinostroit.lit-ry, 1959. 480 p.
(MIRA 12:11)

(Machinery industry)

BOGUSLAVSKIY, Boris L'vovich; GLINKIN, N.M., nauchnyy red.; GORDEYEV, P.A., red.; KOZLOVSKAYA, M.D., tekhn. red.; FERNON, N.N., tekhn. red.

[Semiautomatic and automatic lathes and automatic lines] Tokarnye poluavtomaty, avtomaty i avtomatizirovannye linii. Izd.3., perer. i dop. Moskva, Vses.uchebno-pedagog. izd-vo Proftekhizdat, 1961. 599 p. (MIRA 15:4)
(Lathes) (Automation)

LITVAK, Lev Kisilevich; GLINKIN, N.M., nauchnyy red.; CHI YUN-SHUY
[Ch'ih Yung-shui], red.; FEDERIIY, S.P., tekhn. red.

[Modern methods for drop forging]Sovremennye metody goriachei
shtampovki. Moskva, Proftekhizdat, 1963. 193 p.

(MIRA 16:4)

(Forging)

GLINKIN, N.M.; KOVALEV, K.G.; RUELEV, B.V.

[technical production cards on growing flowering plants
outdoors and under glass] Proizvodstvenno-tekhnologicheskie
karty po vyrashchivaniiu tsvetochnykh rastenii otkryto
i zakrytogo grunta. Moskva, Sirofizdat. Pt.1. 1968. 128 p.
(NII 13-1)

HONDEB, R.M., kadm. kadm. tekhn. nauk, otv. red., AN BSSSR.
A.P., kadm. tekhn. nauk, dots. red.: IELZEL, A.A., kadm.
kadm. tekhn. nauk, red.; NIKOLAYEVICH, V.Ya., dots., red.
GLINKIN, P.P., red.

[Research on construction problems] Issledovaniya po vop-
rosam stroitel'stva. Minsk: Izd-vo Mova speshch, sred-
nego spetsial'nogo i professional'nogo obrazovaniya BSSSR,
1962. 165 p. (MIRA 1814)

1. Minsk. belorusskiy politekhnicheskiy institut.

TSITOVICH, Igor' Sergeyevich; VAVULO, Vasilii Andreyevich; KHVAL', Boris Nikolayevich; GLINKIN, P.P., red.; MORGUNOVA, G.M., tekhn. red.

[Gear wheels of motor vehicles and tractors; design] Zubchatye kolessa avtomobilei i traktorov; proektirovanie i raschet. Minsk, Izd-vo M-va vysshego, srednego spetsial'nogo i professional'nogo obrazovaniia BSSR, 1962. 394 p.

(MIRA 16:4)

(Motor vehicles---Transmission devices) (Gearing)

LENNIK, A. .

Vliianie formy kontura krila na aerodinamicheskie kharakteristiki. Moskva, 1946. 20 p., tables, diagrams. (Izv. A. TsAGI, no. 11)

Bibliography: p. 19.

Title tr.: Effect of wing tip shape on aerodynamic characteristics of the wing.

NOTE: April 1955 no. 174

3 : Aeronautical Sciences and Aviation in the Soviet Union, Library of Congress, 1955

Glinkina, M. I.

Category: USSR/Analytical Chemistry - Analysis of inorganic substances.

G-2

Abs Jour: Referat Zhur-Khimiya, No 9, 1957, 30997

Author : Sinyakova S. I., Glinkina M. I.

Inst : not given

Title : Polarographic Catalytic Molybdenum Current and Its Utilization for Determination of Microgram-Amounts of Molybdenum.

Orig Pub: Zh. analit. khimii, 1956, 11, No 5, 544-552

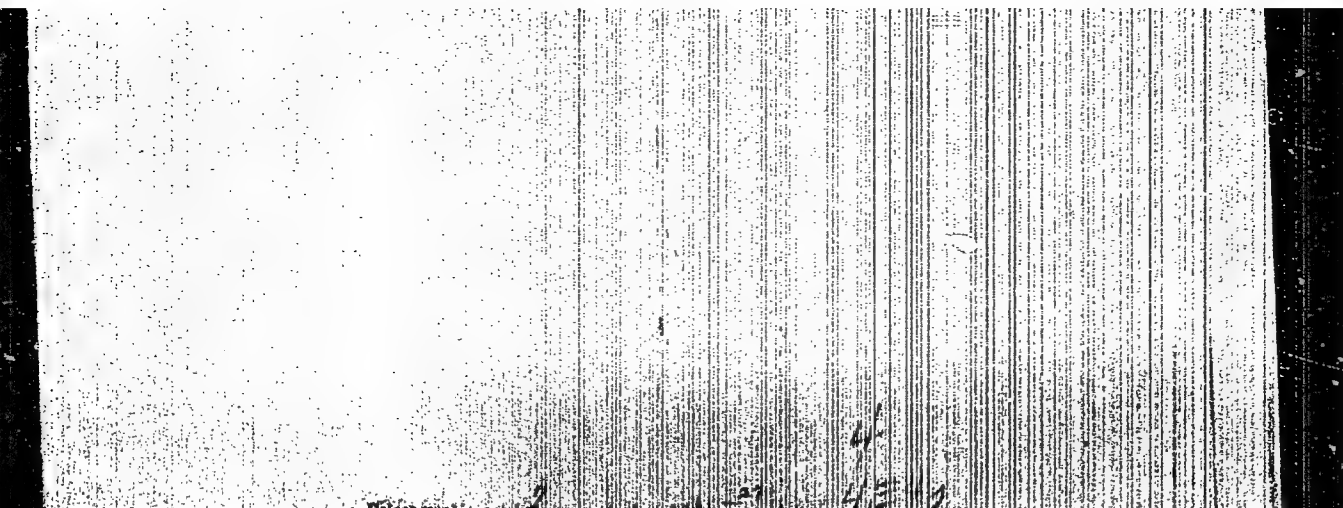
Abstract: Study of the catalytic wave (CW) of Mo with a background of 1 M HClO_4 - 0.75 M H_2SO_4 and 1 M NaClO_4 - 0.75 M H_2SO_4 . It was ascertained that in these media the Mo current does not depend on mercury-column pressure and H_2SO_4 concentration, but depends on concentration of HClO_4 (or NaClO_4) and is due to oxidation of $\text{Mo}(4+)$, which is formed as a result of electrode reduction of $\text{Mo}(5+)$ by the perchloric acid. The possibility is shown of determining the Mo on the basis of the CW, at concentrations up to $1 \cdot 10^{-6}$ M, with a relative error not exceeding $\pm 10\%$.

Card : 1/2

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AUTHORS:

1. V. I. Kiselev, 2. V. I. Kiselev, 3. V. I. Kiselev

TITLE:

Use of Complexes in the Reaction of the Peroxide Ion with Molybdenum
violet (acid) complexes in the presence of molybdenum
or molybdenum complexes (molybdenum
complexes) in the presence of molybdenum
complexes (molybdenum
complexes)

PERIODICAL:

1. V. I. Kiselev, 2. V. I. Kiselev, 3. V. I. Kiselev
(USSR)

ABSTRACT:

In spite of numerous investigations (Refs. 1-3) the mechanism
of the electron reaction of the peroxide ion has not yet
explained. Above all there are up to 10% of the peroxide ion
concerning the nature of the ions of the peroxide ion in the case
of different pH values. The authors of the present paper
show that the molybdate ion (MoO_4^{2-}) exists only in the case of
pH values ≥ 7 whereas in solutions of other acids to a
greater extent the ions H_2MoO_4 , HMoO_4^- , $\text{H}_2\text{MoO}_4^{12}$ are

Card 1/5

MoO_4^{2-} are formed in the case of pH values ≥ 7

Use of Complexones in the Separation of Molybdenum from a Dropping Mercury Electrode in Conjunction with a Dropping Mercury Electrode in Conjunction with a Dropping Mercury Electrode

occur in the solution even in certain cases investigated as described in publications [1-3] with the addition of the molybdate ion in a dropping mercury electrode (DME) in the presence of complex-forming substances (Ligands). In the present paper the results of a study of the behavior of the complex I (nitritotricarbonyl) and complex III (nitritotricarbonyl) in the solution of the styrene diene nitrate (SDN) as well as with several new complexones in conjunction with the fact that (pH concentration of the complex, complex of the mercury column, etc) molybdenum molybdate complex I a well-marked reduction wave in acid solution. The half-wave potential depends on the pH value. In alkaline solutions (pH 8-10) no wave occurs that points to the instability of the complex in alkaline solution. The experimental conditions for the formation of the new complex I at a pH-value of from 4.5 to 9. The reaction of molybdenum with a complicated course is presented in complex I in the case of certain pH values not marked on the graph. Since the amount of the diffusion current is constant in the presence of complex I it is not a good indicator in the pH

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75 11-25/27

Use of Complexes of Polymers with Molybdenum. The Behavior of Molybdenum on a Dropping Mercury Electrode.

-value of the electrode for quantitative determination of molybdenum in the presence of complex III the value of the limiting current of the complex III was found to be independent of the concentration of the complex III and on other conditions. It was found to be the same for the concentration of the complex. In the case of the influence of the pH value it was found that the limiting current in alkaline solution (pH 10) was higher than in acidic solution (pH 1) and increases with increasing pH value. The limiting current reached a maximum at pH 10. The limiting current reached a value of 0.15 mA at pH 10. The limiting current is not suited for determination. The limiting current obtained for molybdenum is not suited for determination, since it depends on the length of the mercury column. The constant of the diffusion current of molybdenum changes with the concentration of molybdenum. In the case of a decrease of the concentration of molybdenum the value of the limiting current of the diffusion

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15-12-1-5/17

Use of Complexones in Polarographic Determination of Molybdenum on a Dropping Mercury Electrode in Complexones

current corresponding to the reduction of Mo(VI) to Mo(III) . In the investigation of the influence of complexones on the polarographic determination of molybdenum, it was found that Fe^{2+} and Cu^{2+} have a limiting current of reduction whereas the ions of Na^+ , K^+ and V^{5+} exerted practically no influence. The reduction of molybdenum in the presence of the disodium salt of aminopolyamine carboxylic compounds in the presence of hexamethylenediamine, triethylenediamine, cyclohexane diamine, ethylenediamine and bis- α -methyl- β -alanine. Summarizing it was found that molybdenum is in all cases reduced in acid solution, whereas in alkaline solution it is formed in alkaline solutions. The limiting current of reduction of molybdenum in the presence of complexones are to a great extent dependent on the volume of the solution of complexone. III gives the best results for analytical purposes. There are 9 figures, 5 tables and 10 references. 22 words in Soviet

Card 4/5

75 13 2 5/27

Use of Complexones in Polarography. Communication II. The Behavior of Molybdenum on a Dropping-Mercury Electrode in Complexones

ASSOCIATION: Institut geokhimii i analiticheskoy khimii im. V. I. Vernadskogo AN SSSR, Moskva
(Moscow Institute of Geochemistry and Analytical Chemistry
imeni V. I. Vernadskiy, AN SSSR)

SUBMITTED: May 27, 1956

1. М. Ю. Устинов, *Современная теория государства и права*, М.: АС-АР, 1999, с. 10.
2. М. Ю. Устинов, *Современная теория государства и права*, М.: АС-АР, 1999, с. 10.

Card 5/5

GLINKIN
LEVINA, S. D.

50V/100V

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Sveshtnik: ly po elektronimam... 4th, Moscow, Russia.
Study...: Isotvoril Transactions of the Berlin Conference...
1969. 388 p. Errata slip inserted. Bibliography annotated.
Sponsorship Agency: Akademika Nauk USSR.
nak.

[illegible]

and G.M. Floriano and T.A. Prusaeva.
Tech. Ed.: T.A. Prusaeva.
PURPOSE: This book is intended for general and specialized students, physicians, nurses, and other health care workers.

COVERAGE: The book contains information on the various aspects of electrochemistry, as well as the physical and chemical aspects of electrochemistry. The book contains information on the various aspects of electrochemistry, as well as the physical and chemical aspects of electrochemistry.

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[illegible][illegible][illegible][illegible][illegible]

...the ... of ...

1. The first step is to identify the problem or question that needs to be answered. This involves understanding the context and the specific requirements of the task.

[illegible]

$\frac{d}{dt} \left(\frac{\partial L}{\partial v^i} \right) = \frac{\partial L}{\partial x^i}$

$$A_{\ell, \ell+1} = \sqrt{\frac{\ell+1}{\ell}} A_{\ell, \ell-1} \quad \text{and} \quad A_{\ell, \ell+1} = \sqrt{\frac{\ell+1}{\ell}} A_{\ell, \ell-1}$$
[illegible]

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S/081/61/000, 019/018/085
B101/B147

AUTHORS: Studenikova, Z. V., Glinkina, M. I., Kornilova, K. I.

TITLE: Geochemistry of tungsten and molybdenum

PERIODICAL: Referativnyy zhurnal. Khimiya, no. 19, 1961, 82, abstract
19G11 (Sb. "Geokhim. tsikly". M., Gosgeoltekhizdat, 1960,
178-186)

TEXT: The authors present extensive material of facts established by them as well as published data characterizing the Mo and W distribution in magmatic rocks. The Mo : W ratio varies between 0.2 and 0.5 in different types of rock. A study of the distribution of these elements in genetically connected series of intrusive rocks showed an accumulation of W in the later border differentiation products (alaskites), with monotonic Mo content and a low increase of its content in basic rocks. Mo separates from W at the stage of formation of quartz diorites (granodiorites). Analytical data of the monomineral fractions show that the principal mass of the two elements is bound to feldspars and quartz, with Mo primarily accumulating in plagioclase. The localization of Mo and W in leucocratic

Card 1/2

Geochemistry of tungsten...

S/081/61/000/010/016/055
B101/B147

minerals is explained by peculiarities of the electronic shells requiring a 6-coordination in the form of a trigonal prism (which can be observed on plagioclase). This leads to an isomorphous substitution of Ca^{2+} . In the autometamorphism of granites, the substitution of plagioclase by muscovite is due to de-anorthositization processes. Ca and W are set free and form small scheelite deposits, primarily in the anticlinal sections of granite massifs. W simultaneously accumulates at the pegmatite stage, and its content in quartz veins decreases. The Mo content in products of postmagmatic processes changes slightly, and increases inconsiderably in the quartz veins. [Abstracter's note: Complete translation.] ✓

Card 2/2

STUDENIKOVA, L. V.: GLINKINA, M. I.: KORNILOVA, K. I.

"Contribution to the geochemistry of tungsten and molybdenum."

Paper submitted at the International Geological Congress XXI Session -
1960 (Reports of Soviet Geologists) Problem No. 1, 15-24 Aug. 61

GLINKINA, V.N.; LAZARSHKO, B.R., doktor tekhn.nauk, nauchnyy red.;
KOVAL'SKAYA, I.F., tekhn.red.

[Electric spark machining of conducting materials; bibliography.
1955-1959] Elektroiskrovaia obrabotka tokoprovodiashchikh
materialov; bibliograficheskii ukazatel', 1955-1959. Moskva,
1960. 68 p. (MIRA 13:11)

1. Akademiya nauk SSSR. Tsentral'naya nauchno-issledovatel'skaya
laboratoriya elektricheskoy obrabotki materialov. 2. Nauchno-
tekhnicheskaya biblioteka Tsentral'noy nauchno-issledovatel'skoy
laboratorii elektricheskoy obrabotki materialov AN SSSR (for
Glinkina).

(Bibliography--Electric metal cutting)

Veterinary Medicine

Work of the Moscow Veterinary Academy. Veterinariia 29 no. 6, 1952.

Monthly List of Russian Accessions, Library of Congress, August 1952. Unclassified.

AUTHOR: Leproskiy, V.V., Kapustin, S.A., Glinkov, I.M. and
Slepkanov, P.N. 133-5-6/27

TITLE: On the comparison of tilting and fixed open hearth
furnaces. (O sravnenii kachayushchikhsya i statsionarnykh
martenovskikh pechey.)

PERIODICAL: "Stal'" (Steel), 1957, No. 5, pp. 411-413 (U.S.S.R.)

ABSTRACT: This paper is a comment on the paper by K.G. Trubin,
"Stal'", 1956, No.9. The above subject is discussed in the
light of the results of operating 250 ton tilting furnaces on
the Azovstal' Works. For comparison with fixed furnaces the
results obtained on the Zaporozhstal' Works are quoted. After
indicating that the bottoms of tilting furnaces require more
maintenance the authors compare the productivity of both types
of furnaces. The dependence of the output per hour on the
bottom surface (Fig. 1) and on furnace capacity (Fig.2) indi-
cates that for furnaces of the same bottom area and the same
capacity the productivity of fixed furnaces is better. Ther-
mal efficiency of tilting and fixed furnaces is compared on
the basis of heat losses and the extent of preheating of gas
and air (Fig. 3). The stability of roof refractories in tilt-
ing furnaces is lower than in fixed ones; Azovstal' - 29
kg/ton of steel while on the Makeyevsk Works - 20 kg/ton. It
is concluded that technical-economical indices of tilting

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On the comparison of tilting and fixed open hearth furnaces.
(Cont.)

133-5-6/27

furnaces are somewhat lower than those of fixed ones. A comparatively flexible slag operation of tilting furnaces is acknowledged, however, the removal of the first slag starts in the period of the maximum activity of the bath, when the composition of slag has not reached an optimum. In this respect the operation is similar to one on fixed furnaces. There are 4 figures and 5 references, 4 of which are Slavic.

ASSOCIATION: Azovstal' Works and Zhdanovsk Metallurgical Institute.
(Zavod Azovstal' i Zhdanovskiy Metallurgicheskii Institut.)

AVAILABLE:

Card 2/2

SOV, 137-58-9-18607 D

Translation from: Referativnyy zhurnal, Metallurgiya, 1956, Nr 9, p 63 (USSR)

AUTHOR: Glinkov, G.M.

TITLE: The Heat Absorption of an Open-hearth-furnace Bath as a Basic Parameter of the Control of its Thermal Performance (Teplo-pogloshcheniye vanny martenovskoy pechi kak osnova regulirovaniya teplovoy raboty)

ABSTRACT: Bibliographic entry on the author's dissertation for the degree of Candidate of Technical Sciences, presented to the Mosk. in-t stali (Moscow Institute of Steel Industry), Moscow, 1958

ASSOCIATION: Mosk. in-t stali (Moscow Institute of Steel Industry), Moscow
1. Furnaces--Performance 2. Material--Thermochemistry

Card 1/1

SOV/137-58 9 18569

Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 9, p 56 (USSR)

AUTHORS: Kapustin, Ye. A., Makovskiy, V. A., Glinkov, G. M.

TITLE: The Role of Oxygen-enriched Flame in Oxidation Processes of Open-hearth Smelting (Rol' obogashchennogo kislorodom fakela v okislitel'nykh protsessakh martenovskoy plavki)

PERIODICAL: Izv. vyssh. uchebn. zavedeniy. Chernaya metallurgiya, 1958, Nr 9, pp 84-92

ABSTRACT: An experimental campaign carried out in a 170-ton open hearth furnace of the "Azovstal'" plant has shown that increased consumption of O_2 in the flame increases the oxidation capacity of the furnace, the oxidation capacity being defined as the passage of O_2 into the molten metal per unit of time. It was noted that the boundary of the visible brightly luminous flame is sharply reduced when O_2 is introduced. Thus, at an O_2 consumption of 2500 m³/hr the length of the flame is reduced to one-half of the length of the hearth. Gas samples taken along the length of the hearth revealed that uncombusted components (CO , H_2) are found only within the boundaries of the visible flame. At high rates of fuel

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SOV/137 58 9 18569

The Role of Oxygen-enriched Flame (cont.)

combustion and during frequent reversals (8-12 minutes), smaller quantities of combustible constituents are found in the central section of the furnace and it is for this reason that the gaseous phase attains its maximum oxidizing capacity in this area. The flame exhibits a maximum temperature near the first charge opening and a minimum temperature in the vicinity of the fifth opening (the temperature drop may be as great as 150-250°C). Analyses of the slag have indicated that the greatest content of Fe in the slag is found in the center of the furnace, in the vicinity of the nozzles, where conditions are favorable for the passing of Fe into the slag; this conclusion was fully substantiated by experiment. The thermal balance of the smelting process is very favorably affected when a portion of the oxygen of the ore or of the colder is replaced by atmospheric oxygen. Thus, every ton of O_2 absorbed from the furnace atmosphere reduces the amount of heat required for preheating and fusion by approximately 5 million kcal.

1. Open hearth furnaces—performance 2. Fuel—consumption
3. Oxygen—performance 4. Slag—analysis

Yu. N.

Card 2/2

164-54-6-9/19
The Temperature of the Combustion Products at the Working Space of a Tilting Combustion Engine

ASSOCIATION: Zhukovskiy A. G. (Zukhovskiy A. G.)
Soviet "Aerostats" (Zhukovskiy A. G. (Zukhovskiy A. G.)
and "Aerostats" (Zhukovskiy A. G. (Zukhovskiy A. G.))

AVAILABLE: Library of Congress

Card 2/2

133-58-4-33/40

AUTHOR: GILBERT, G. E.

TITLE: Control of Heating Conditions by Maintaining the Maximum Heat Absorption of an Open Hearth Bath (Regulirovaniye teplovygo rezhima poldovzheniyei maksimall'nogo teploabsorbirovaniya v otkryt'yei pechi)

PERIODICAL: Stal', 1958, Nr 4, pp 470-478 (USSR)

ABSTRACT: The possibility of a static and simple determination of the value of the specific absorption of heat by the bath and the coefficient of useful action of an open hearth furnace was investigated. In order to utilise the value of heat absorption by the bath in order to control the thermal operation of an open hearth furnace, it was necessary to devise a rapid method of determination of the mean heat absorption of the bath at frequent but short time intervals. A method of instantaneous reciprocal heat balance developed by VNIIM (Ref.7) was tried. Specific heat consumption of the bath (cal/m² hr) is calculated from a general formula:

$$q = \frac{Q_x + Q_f + Q_{TO} - Q_{yx} - Q_{loss}}{F}$$

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133-58-4-33/40

Control of Heating Conditions by Maintaining the Maximum Heat
Absorption of an Open Hearth Bath

where: Q_x - chemical heat of fuel;
 Q_f - physical heat of fuel and air;
 Q_{CO} - heat of combustion of CO from the bath;
 Q_{yx} - heat leaving the working space with waste gas;
 q_{los} - losses of idling;
 F_2 - surface area of the bottom, m^2 .

In order to find out the nature of changes of heat absorption in the course of the heat and its dependence on various factors 15 experimental heats were carried out on a 350 ton tilting furnace (Azovstal' Works) with a magnesite chromite roof operating with a high phosphorus pig (P 1.4-1.7%) with 72-77% of hot iron in the charge. In order to determine the heat absorption by the bath by the method of instantaneous heat balance, the following measurements were carried out:

a) temperature of preheat of air using a suction thermo-couple in the vertical flue on a level 1 m above the

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133-59-4-33/40

Control of Heating Conditions by Maintaining the Maximum Heat
Absorption of an Open hearth Bath

platform, every 15-20 min;
b) temperature of gas preheat with a suction thermocouple;
c) temperature of waste gas. The latter was measured every 15-20 min in the air vertical flue in the same place where the air temperature was measured. A thermocouple was introduced 40-50 cm deep for 30-40 sec. The indications of this thermocouple were tested with a suction thermocouple and found to be satisfactory. Using the above three temperatures and indication of instruments on the consumption of fuel and air, the specific heat absorption and the coefficient of useful action were calculated for each heat. The experimental heats were done under various thermal and oxygen conditions. The results are shown in Fig.1 and the Table (for two heats). A comparison of heat balances obtained from the heat absorption curve and calculated for the whole heat indicated that the accuracy of instantaneous heat balances is about 10%. The dependence of heat absorption: on thermal load - Fig.2, on the rate of charging of granular materials (Fig.3A) and on the thermal load

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Control of Heating Conditions by Maintaining the Maximum Heat
Absorption of an Open Hearth Bath

133-58-4-33/40

during melting - Fig.3B, on the velocity of decarburisation - Fig.4. It was established that the air and waste gas temperature can be determined from measurements of the temperature of the internal surface of the wall of the vertical flue with a radiation pyrometer (Figs.5,6). It is pointed out that it would be advantageous to design a scheme for a complete automatic control for open hearth furnaces, using as the main controlling parameter the specific consumption of heat by the bath which completely defines the thermal operation of the furnace. The method described in the paper is suitable for instrumentation and thus can form a basis for developing an automatic control for open hearth furnaces. The work was carried out under the direction of I. G. Kazantsev, Professor, Doctor of Technical Science. There are 1 table, 4 figures and 8 references, 7 of which are Soviet, 1 English.

Card 4/4

1. Open hearth furnaces--control systems

SCV/133-58-2-2/30

AUTHORS: Kharitonov, A.S., Candidate of Technical Sciences, Docent,
Bul'skiy, M.T., Alimov, A.G., Glinkov, G.E. and
Beloglazovskiy, M.Sh., Engineers

TITLE: Optimum Temperature Conditions for Smelting Rimming Steel
from Phosphorus Pig Iron (Optimal'nyy temperaturnyy rezhim
vyplavki kipyashchey stali iz fosforistogo chuguna)

PERIODICAL: Stal', 1958, No 8, pp 706 - 709 (USSR)

ABSTRACT: An outline of the smelting practice of rimming steels used
in the Azovstal' Works is given. On the basis of an
analysis of the temperature data during the refining
period of a large number of heats, the optimum metal temper-
ature at the beginning of boiling and before deoxidation
was established in order to obtain steel with a low
consumption coefficient. The influence of the charging
rate of additions during the refining period on the
velocity of heating of metal - figure 1; the influence of
the metal temperature at the beginning of pure boiling
on the number of ladles of metal of low and high con-
sumption coefficients - Figure 2; the influence of metal
temperature before deoxidation on the number of ladles of
metal of high and low consumption coefficients - Figure 3;

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Optimum Temperature Conditions for Smelting Steel from
Phosphorus Pig Iron

the influence of the $[Mn] : [C]$ ratio in the finished
rimming steels on the absorption coefficient of metal -
Figures 4 and 5 (A): Frequency distribution of the number
of ladles of steel with different $[Mn] : [C]$ ratios -
Figure 5 (B). It was also established that it is advantage-
ous to produce rimming steel with the manganese content
in the ladle sample near to the lower limit permitted by
standards and that the ratio of $[Mn] : [C]$ in the finished
steel should not exceed 2.7 for steels StC, 1 and 2kp and
2.5 for steel St3kp. There are 5 figures and 3 Soviet
references.

ASSOCIATIONS: Zhdanovskiy metallurgicheskiy institut (Zhdanov
Metallurgical Institute) and Zavod "Azovstal'"
("Azovstal'" Works)

Card 2/2

- Steel--Production 2 Steel--Temperature Factors

GLINKOV, G.M. kand. tekhn. nauk

Heat exchanges in open hearth furnace smelting chambers. Izv.
vys.ucheb.zav.; Chern.met. no.10:69-74 O '58. (MIRA 11:12)

1. Zhdanovskiy metallurgicheskii institut.
(Open-hearth furnaces) (Heat--Transmission)

GLINKOV, G.M., kand. tekhn. nauk.

Feasibility of using computing devices for the automatization
of open-hearth furnaces. Izv. vys. ucheb. zav.; Chern. met. no.12:
51-55 D '58. (MIRA 12:3)
(Open-hearth furnaces) (Automatic control)

SOV 137 58 11 22682

Translation from: Referativnyy zhurnal Metallurgiya 1958, Nr 11 p 36 (USSR)

AUTHOR: Glinkov, G M.

TITLE: Heat Absorption in the Bath of an Open hearth Furnace During a Heat as the Basis for Regulation of Thermal Conditions (Teplopegloshcheniye vanny martenovskoy pechi po khodu plavki kak osnova dlya regulirovaniya teplovoi raboty)

PERIODICAL: Sb. Mosk. in t stal: 1958, Vol 38 pp 112-134

ABSTRACT: Change in heat absorption (H) of the bath was determined for the courses of 15 experimental heats in 350 t tilting open hearth furnaces at the Azovstal' plant equipped with chemically bonded magnesite chrome roofs two level checker ports heated by a mixture of coke and blast-furnace gases, and burning in an oxygen enriched blow. The method of measurement is described. Comparisons showed that the difference between the quantity of heat received by the bath and calculated on the total heat balance and the same quantity of heat calculated by the method of inverse heat balance for one heat was 2 and for another 10.5 million kcal, constituting altogether 2.8 and 13.5% of the total heat output. The amount of H varies highly in the

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SOV 197 56 11 1980

Heat Absorption in the Bath of an Open hearth Furnace During a Heat

course of a heat. Ranging from an average of 150-180,000 kcal/m³ hr during the charging period (180-220,000 during charging of iron scrap and blooms), 60-80,000 at the end of the meltdown period, 100-140,000 at the start of the melting period, 60-80,000 at the end of the melting period and fluctuating in the range of 40-70,000 during the finishing period. During charging, melting down and melting, H rises with increase in O₂ consumption. The average for two groups of heats showed that when O₂ delivery was increased from 1500 to 2500 m³/hr H rose from 153 to 186,000 kcal/m³ hr during the charging period, from 118 to 149,000 kcal/m³ hr during the meltdown period. H rises with increases in thermal load, the rise being the greater during the charging period the greater is the O₂ input. At identical thermal conditions, H during the period of charging of free flowing materials rises with the rate of charging. No such relationship was observed during the period of charging the metallic portion of the charge. The change in the efficiency of the furnace during the heat (an analogous change in H) is as follows: Charging 33.1-37.0%, meltdown 28.0-31.4%, melting 18.4-20.6% and finishing 12.8%. Since the change in the H and the efficiency of the furnace during the heat provide a complete description of the thermal functioning of the furnace, the utilization of the H of the bath or the efficiency of the furnace as input control impulses permits the development of new designs for automatic regulation of the thermal regimes of furnaces furnishing

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SOV 17 58 11 1981

Heat Absorption in the Bath of an Open hearth Furnace During a Heat (cont.)

computers), thereby permitting a pronounced intensification of the thermal functioning of the furnace.

X 1

Card 3/3

307/148-59-1-9/19

18(5)

AUTHORS: Kapustin, Ye.A., Glinkov, G.M., Candidates of Technical Sciences and Kaluzhskiy, Ye.A., Engineer

TITLE: Raising the Productivity and Economy of Open Hearth Furnace by Improving the Thermal Process (Povysheniye proizvoditel'nosti i ekonomichnosti martenovskoy pechi za schët usovershenstvovaniya teplovogo rezhima)

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy - Chernaya metallurgiya, 1959, Nr 1, pp 83-89 (USSR)

ABSTRACT: Experiments were carried out for the purpose of developing an improved heat process in open hearth furnaces, whereby optimum correlation of blast air and mazut consumption during the smelt were determined. The following personalities participated in the work: A.A. Goshchanskiy, V.I. Doroknov, V.P. Yevtyukhov, D.P. Zabrodin, V.F. Kalinkin, A.Ye. Prikozhenko, V.D. Rudman, A.A. Rykhlikova, N.G. Stepin, I.S. Chernyshev. It was stated that the determination of the blast expense depended on the components of air balance such as: air expense for fuel burning, oxidation of the pool, burning-out of CO, as well as loss of air caused by leakages and air intake from the external space.

Card 1/2

SOV/143-59-1-9/19

'Raising the Productivity and Economy of Open Hearth Furnace by Improving the Thermal Process

Air intake and loss depended on the pressure in the smelting space. For the case that optimum pressure under the smelting space coupola could not be maintained, the blast expense must be adjusted accordingly. The developed thermal process regulates the thermal load depending on the charge material (loose or scrap); the quality of the scrap; duration of initial heating and idle time; and the smelting intensity. The new method reduced the smelting time by 6.4% and the specific fuel expense by 8.3%. The author presents graphs where the mazut expense is plotted versus the smelting time; the quantity of beads and the Fe-content in the slag; etc.

There are 8 graphs and 6 Soviet references.

ASSOCIATION: Zhdanovskiy metallurgicheskii institut (Zhdanov Metallurgical Institute)

SUBMITTED: October 1, 1958

Card 2/2

SV/153-59-6-77/41

AUTHORS: Glinkov, M.A., Doctor of Technical Sciences and
Glinkov, G.M., Candidate of Technical Sciences

TITLE: Some Thermotechnical Problems of Large Capacity Open
Hearth Furnaces (Nekotoryye voprosy teplotekhniki
bol'shegruznykh martenovskikh pechey)

PERIODICAL: Stal', 1959, Nr 6, pp 568-572 (USSR)

ABSTRACT: Possibilities of increasing the productivity of open
hearth furnaces per unit of their capacity is
discussed. It is considered that the higher the
furnace capacity, the higher the quality of the solid
charge should be. This would permit retaining the
level of irradiation factor on decreasing of the
ratio of the surface area of the bath to the furnace
capacity (S/T). The higher the furnace capacity the
higher the quality of the liquid iron or semiproduct
should be as an increase in the thickness of the slag
layer unavoidably deteriorates conditions of heat
transfer. Sufficiently advantageous heat exchange
conditions inside the solid charge and liquid bath can
be obtained on retaining S/T constant with increasing

Card 1/4

504/137-59-6-37/41

Some Thermotechnical Problems of Large Capacity Open Hearth
Furnaces

furnace capacity. In order to obtain this a different type of steelmaking furnace is necessary - with a working space up to 10 - 12 m wide, hanging roof and two-sided charging (with a corresponding change in the distribution of equipment in the shop). The higher is the laying down property of the flame and its luminosity at the end of the smelting space the lower is non-uniformity in the heat exchange along the length of the furnace. Therefore on increasing the capacity of the furnaces, it is necessary to increase correspondingly the velocity of the fuel stream in order to obtain the required laying down capacity of the flame. In order to improve the flame luminosity at the end of the smelting space, it is necessary to use as a fuel or a carburising agent, heavy liquid fuels with a large ratio of C/H, on the decomposition of which complex hydrocarbon complexes are formed, securing stable luminosity of the flame.

Card 2/4

SOV/133-79-6-37/11

Some Thermotechnical Problems of Large Capacity Open Hearth
Furnaces

A truly uniform heating of the baths of large furnaces can be obtained with a two-sided supply of fuel into the working space i.e. with simultaneous operation of two dog houses. On transferring an open hearth furnace on firing with oil or a cold gas of a high calorific value this problem can be solved easily by using three-channel dog houses (Fig 5). In each dog house either two side-channels or one central channel operates alternatively. The remaining three channels serve as waste gas flues to pass the waste gas to the regenerators - simultaneously through both dog houses. The movement of the gas in the working space will be mixed (counter-current and recirculation). As each dog house supplies through tuyeres the same amount of fuel, the heating conditions of both halves of the working space should be the same. All four regenerators are preheating air, the reversing system will be little changed. The separation of slag in slag pockets will be facilitated as due to the peculiar

Card 3/4

SOV/133-59-6-37/41

Some Thermotechnical Problems of Large Capacity Open Hearth
Furnaces

feature of the gas movement in the working space
the carry over of the slag decreases. There are
5 figures and 9 Soviet references.

Card 4/4

KRIVANDIN, Vladimir Alekseyevich; GLINEOV, G.M., red.; VAGIN, A.A.,
red.izd-va; EVENSON, I.M., tekhn.red.

[Ceramic recuperators] Keramicheskie rekuperatory. Moskva,
Gos.nauchno-tekhn.izd-vo lit-ry po chernoi i tsvetnoi
metallurgii, 1960. 171 p. (MIRA 13:2)
(Heat exchangers)

LEPORSKIY, Vladimir Vladimirovich; KAPUSLIN, Yevgeniy Aleksandrovich;
GLINKOV, German Markovich; MAKOVSKIY, Vitaliy Anato'lyevich;
LEBEDEV, A.I., red.; LANOVSKAYA, M.R., red. ind-va; DOBUZEIN-
SKAYA, L.V., tekhn.red.

[Tilting open-hearth furnaces; design and heat transfer] Ka-
chainushchiasia martenovskia pech'; konstruksia i teplovaia
rabots. Moskva, Gos.nauchno-tekhn.izd-vo lit-ry po chernoi i
tsvetnoi metallurgii, 1961. 181 p. (MIRA 14:5)
(Open-hearth furnaces--Design and construction)
(Heat--Transmission)

GLINKOV, G.M.; PALOSHIN, N.A.; KAFUSTIN, Ye.A.; KARFIM, G.D.; RODMAN, V.D.;
KHIISH, I.I.

Results of modeling open-hearth furnaces fired by cold high-calorie
gas and hot mixed gas. Izv. vys. uchet. zav.; Chern. met. no.2:
138-147 '61. (MIRA 14:11)

1. Zhdanovskiy metallurgicheskiy institut.
(Open-hearth furnaces--Models)
(Gas flow--Models)

GLINKOV, M.A., doktor tekhn.nauk,prof.; GLINKOV, G.M., kand.tekhn.nauk

Response to A. D. Kliuchnikov's remarks. Stal' 21 no.6:566 Je '61.
(MIRA 14:5)

(Open-hearth furnaces--Design and construction)

GLINKOV, M.A.; GLINKOV, G.M.

Role of heat generation in open-hearth furnaces.
Stal' 21 no.8:751-753 Ag '61. (MIRA 14:9)
(Open-hearth furnaces)

LEPORSKIY, V.V.; SLEPKANOV, P.M.; ARKHANGEL'SKIY, Ye.N.; POPOL'SKAYA,
G.A.; GLINKOV, G.M.; KAPUSTIN, Ye.A.; KALOSHIN, N.A.; KRIVENKO, P.T.

Operation of large tilting open-hearth furnaces with natural gas.
Stal' 21 no.10:883-889 O '61. (MIRA 14:10)

1. Zavod "Azovstal'" i Zhdanovskiy metallurgicheskiy institut.
(Open-hearth furnaces)

KAPUSTIN, Yevgeniy Aleksandrovich; GLINKOV, German Markovich; MITKALINNY, V.I., dots., retsenzent; GOLYATKINA, A.G., red. izd-va; KAPASEV, A.I., tekhn. red.

[Flow of gases in open-hearth furnaces] Dvizhenie gazov v martenovskikh pechakh. Moskva, Metallurgizdat, 1963. 270 p.
(MIRA 16:4)

(Open-hearth furnaces) (Gas flow)

PHASE I BOOK EXPLOITATION

334/5556

84-

Moscow. Institut stali.

Novoye v teorii i praktike proizvodstva martenovskoy stali (New [Developments] in the Theory and Practice of Open-Hearth Steelmaking) Moscow, Metallurgizdat, 1961. 459 p. (Series: Trudy Mezhdunarodskogo nauchnogo soveshchaniya) 2,150 copies printed.

Sponsoring Agency: Ministerstvo vysshego i srednego spetsial'nogo obrazovaniya RSFSR. Moskovskiy institut stali imeni I. V. Stalina.

Eds.: M. A. Glinkov, Professor, Doctor of Technical Sciences, V. V. Kondakov, Professor, Doctor of Technical Sciences, V. A. Kudrin, Docent, Candidate of Technical Sciences, G. N. Oyko, Professor, Doctor of Technical Sciences, and V. I. Yavovskiy, Professor, Doctor of Technical Sciences; Ed.: Ye. A. Borko; Ed. of Publishing House: N. D. Gromov; Tech. Ed.: A. I. Karasev.

PURPOSE: This collection of articles is intended for members of scientific institutions, faculty members of schools of higher education, engineers concerned with metallurgical processes and physical chemistry, and students specializing in these fields.

Card 1/14

New [Developments] in the Theory (Cont.)

SOV/5556

COVERAGE: The collection contains papers reviewing the development of open-hearth steelmaking theory and practice. The papers, written by staff members of schools of higher education, scientific research institutes, and main laboratories of metallurgical plants, were presented and discussed at the Scientific Conference of Schools of Higher Education. The following topics are considered: the kinetics and mechanism of carbon oxidation; the process of slag formation in open-hearth furnaces using in the charge either ore-lime briquets or composite flux (the product of calcining the mixture of lime with bauxite); the behavior of hydrogen in the open-hearth bath; metal desulfurization processes; the control of the open-hearth thermal melting regime and its automation; heat-engineering problems in large-capacity furnaces; aerodynamic properties of fuel gases and their flow in the furnace combustion chamber; and the improvement of high-alloy steel quality through the utilization of vacuum and natural gases. The following persons took part in the discussion of the papers at the Conference: S.I. Filippov, V.A. Kudrin, M.A. Glinkov, B.P. Nam, V.I. Yavovskiy, G.M. Oyka and Ye. V. Chelishchev (Moscow Steel Institute); Ye. A. Kazachkov and A. S. Kharitonov (Zhdanov Metallurgical Institute); N.S. Mikhaylets (Institute of Chemical Metallurgy of the Siberian Branch of the Academy of Sciences USSR); A.I. Stroganov and D. Ye. Povolotskiy (Chelyabinsk Polytechnic Institute); P.V. Umrikhin (Ural Polytechnic Institute); I.I. Fomin (the Moscow "Serp i Molot" Metallurgical Plant); V.A. Foklev (Central Asian Polytechnic Institute).

Card 2/14

New [Developments] in the Theory (Cont.)

ECV/5555

and M.I. Beylinov (Night School of the Dneprodzerzhinsk Metallurgical Institute).
References follow some of the articles. There are 268 references, mostly Soviet.

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Principal Trends in the Development of Scientific Research in Steel
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Institute]. Regularity Patterns of the Kinetics of Carbon Oxidation
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[V. I. Antonenko participated in the experiments]

Levin, S. L. [Professor, Doctor of Technical Sciences, Dnepropetrovskiy
metallurgicheskii institut - Dnepropetrovsk Metallurgical Institute].

Card 3/14

New [Developments] in the Theory (Cont.)

SOV/5556

Gol'dfarb, E.M. [Candidate of Technical Sciences, Dnepropetrovsk Metallurgical Institute]. Introduction to the Similarity Theory of Open-Hearth Furnaces

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Protopopov, V.S. [Engineer, Kuznetskiy metallurgicheskii kombinat - Kuznetsk Metallurgical Combine]. Special Features of the Operation of High-Capacity Open-Hearth Furnaces

249

Glinkov, G.M. [Candidate of Technical Sciences, Zhdanovskiy metallurgicheskii institut - Zhdanov Metallurgical Institute]. Heat-Engineering Problems of High-Capacity Open-Hearth Furnaces

253

Ivanov, N.I. [Docent, Candidate of Technical Sciences], V.F. Gazhur, and V.I. Shakhlin [Engineers], [Magnitogorskiy metallurgicheskii kombinat - Magnitogorsk Metallurgical Combine; Magnitogorskiy gorno-metallurgicheskii institut - Magnitogorsk Mining and Metallurgical Institute]. Theoretical Principles of the Unit-Block System in the Design of Open-Hearth Furnaces

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Card 9/14

L 17595-65 EWT(d)/EWT(m)/EWP(c)/EWA(d)/EWP(v)/T-2/EWP(t)/EWP(k)/EWP(h)/EWP(l)
 ACCESSION NR AM4046730 BOOK EXPLOITATION Pf-4 MLK/JD/ 5/

Samarin, A. M., ed. (Corresponding member, Academy of Sciences, U.S.S.R.) 84/

Steel production; handbook (Staleplavil'noye proizvodstvo: spravochnik),
 t. 2., Moscow, Izd-vo "Metallurgiya", 1964, 1039 p. illus., biblio.,
 tables. Errata slip inserted. 5,850 copies printed.

TOPIC TAGS: steel, open-hearth furnace, quality control, refractory

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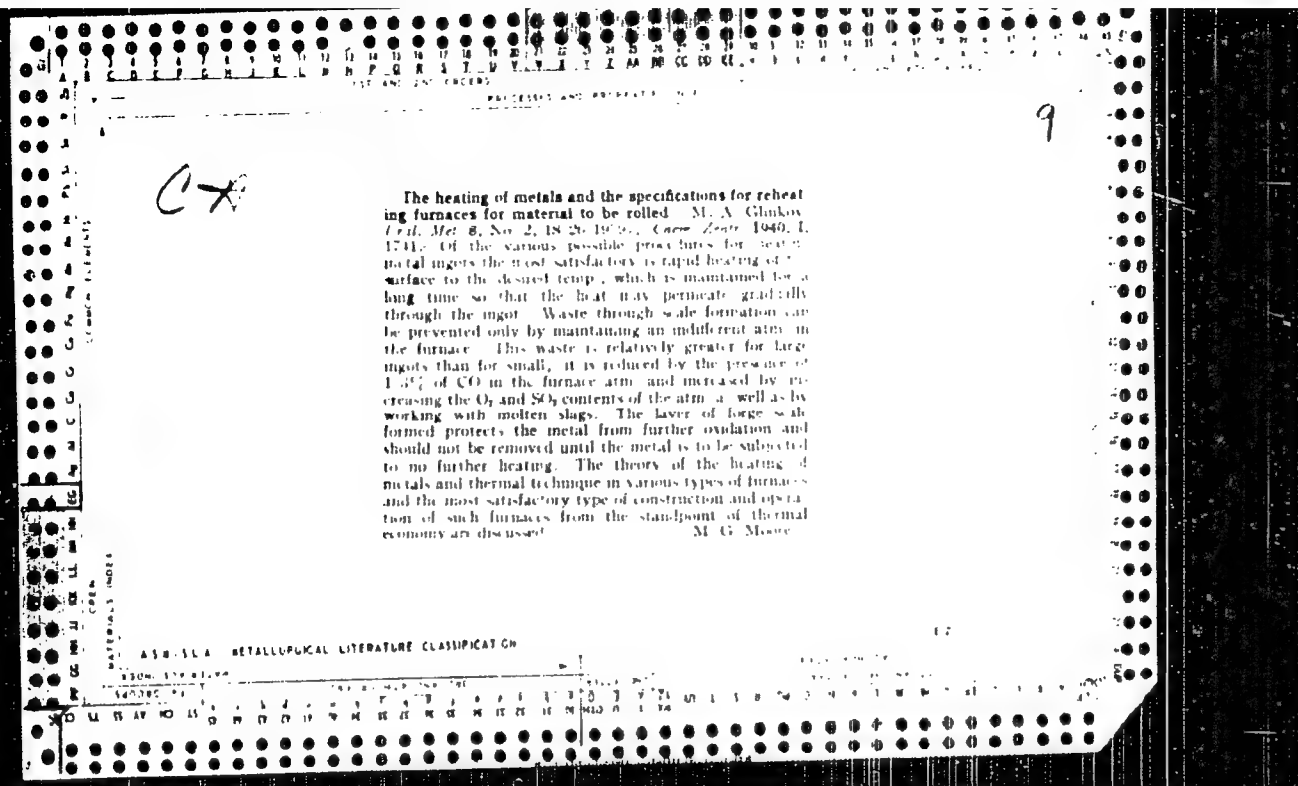
SUB CODE: MM

OTHER: 030

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NR REF SOV: 279

Card 3/3



Some Remarks About the Theory and Design of Open-Hearth Furnaces. M. Glinkov. (Stal, 1940, No. 3, pp. 16-20) (In Russian). The first section is devoted to a consideration of the

heat transfer and heat balance in the working space of an open-hearth furnace. Some expressions for heat transfer are derived and the effect of the presence of either the solid or molten charge on heat transfer is considered. Temperature conditions and heat distribution in the working space are considered in the next section. Limits are imposed by refractoriness of the lining, but the temperature of the flame should be as high as possible. To obtain a constant surface temperature of the lining, the temperature of the gases should be higher the lower the temperature of the metal and the lower the ratio of the surface area of the lining to the surface area of the charge. For melting, the higher the temperature of the flame for a constant temperature of the lining the better. The intensity of heat exchange in the working space will be the greater the smaller the temperature gradient along the length of the flame. The higher (within limits) the temperature of the exit gases. It is stated that with insulated furnace roofs there is no need to have a lower flame temperature, but pyrometric equipment should be installed to check roof temperatures. In the concluding section the geometry of the working space is discussed.

ADA 514 METALLURGICAL LITERATURE CLASSIFICATION

CA 9

The hydrodynamics and heat exchange in the steel bath of the open hearth. M. A. Glukov. *Ural. Mez.* 9, No. 9, 15 19(1940). *Chem. Zentr.* 1941, II, 801. Theoretical discussion of the thermodynamics and heat-exchange processes in the steel bath of the open hearth and the significance of the theoretical knowledge of such processes with respect to the construction and technological aspects of steel manuf. It was established that no rules can be set down regarding the influence of such processes on the course of melting. H. Stoertz

ASB-SLA METALLURGICAL LITERATURE CLASSIFICATION

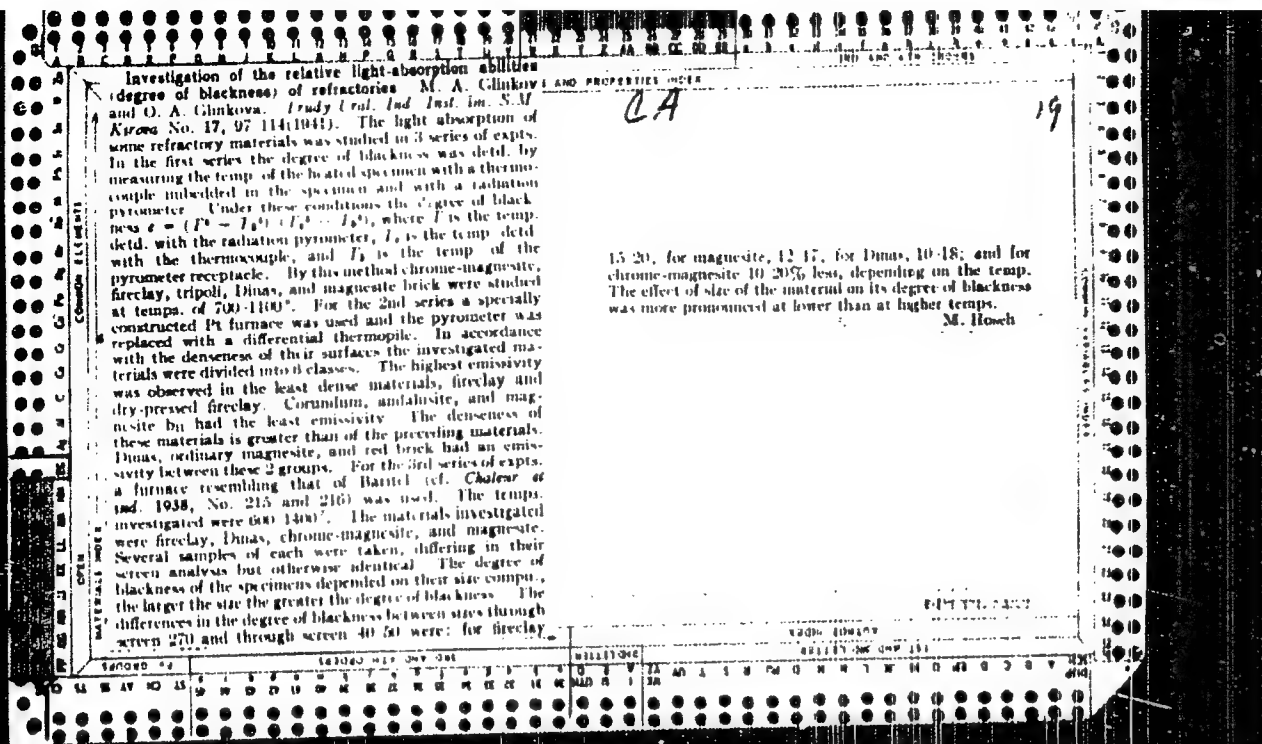
| 117 AND 120 GROUPS | | PROCESS AND PROPERTY INDEX | |
|--|--|----------------------------|--|
| <p>1225. INVESTIGATION OF THE RELATIVE LIGHT ABSORPTION ABILITY (DEGREE OF "BLACKNESS") OF REFRACTORIES. Glinkov, V.A. and Glinkova, O.A.. (Trudy Ural. Ind. Inst. im. S.M. Kirova, 1941, No. 7, 97.114). The light absorption of some refractory materials was studied in 3 series of experiments. In the first series the degree of blackness was determined by measuring the temperature of the heated specimen with a thermo couple imbedded in the specimen and with a radiation pyrometer. Under these conditions the degree of blackness $\alpha = (T^4 - T_b^4) / (T_s^4 - T_b^4)$, where T is the temperature determined with the radiation pyrometer, T_s is the temperature determined with the thermo couple, and T_b is the temperature of the pyrometer receptacle. By this method chromomagnesite, fireclay, tripoli, dinas, and magnesite brick were studied at temperatures of 700-1100°. For the 2nd series a specially constructed Pt furnace was used and the pyrometer was replaced with a differential thermopile. In accordance with the denseness of their surfaces the investigated materials were divided into 3 classes. The highest emissivity was observed in the least dense materials.</p> | | | |
| <p>ASB-5LA METALLURGICAL LITERATURE CLASSIFICATION</p> | | | |
| <p>122500 122500</p> | | <p>122500 122500</p> | |

fireclay and dry pressed fireclay. Corundum, andalusite, and magnesite had the least emissivity. The denseness of these materials is greater than of the preceding materials. Limes, ordinary magnesite, and red brick had an emissivity between these 2 groups. For the 3rd series of experiments a furnace resembling that of Baritel was used. The temperatures investigated were 800-1400°. The materials investigated were fireclay, Dinas, chromemagnesite, and magnesite. Several samples of each were taken, differing in their screen analysis but otherwise identical. The degree of blackness of the specimens depended on their size composition, the larger the size the greater degree of blackness. The differences in the degree of blackness between sizes through screen 270 and through screen 40-50 were: for fireclay 15-20; for magnesite, 12-17; for Dinas, 10-15; and for chromemagnesite 10-20% less, depending on the temperature. The effect of size of the material on its degree of blackness was more pronounced at lower than at higher temperatures.

C.A.

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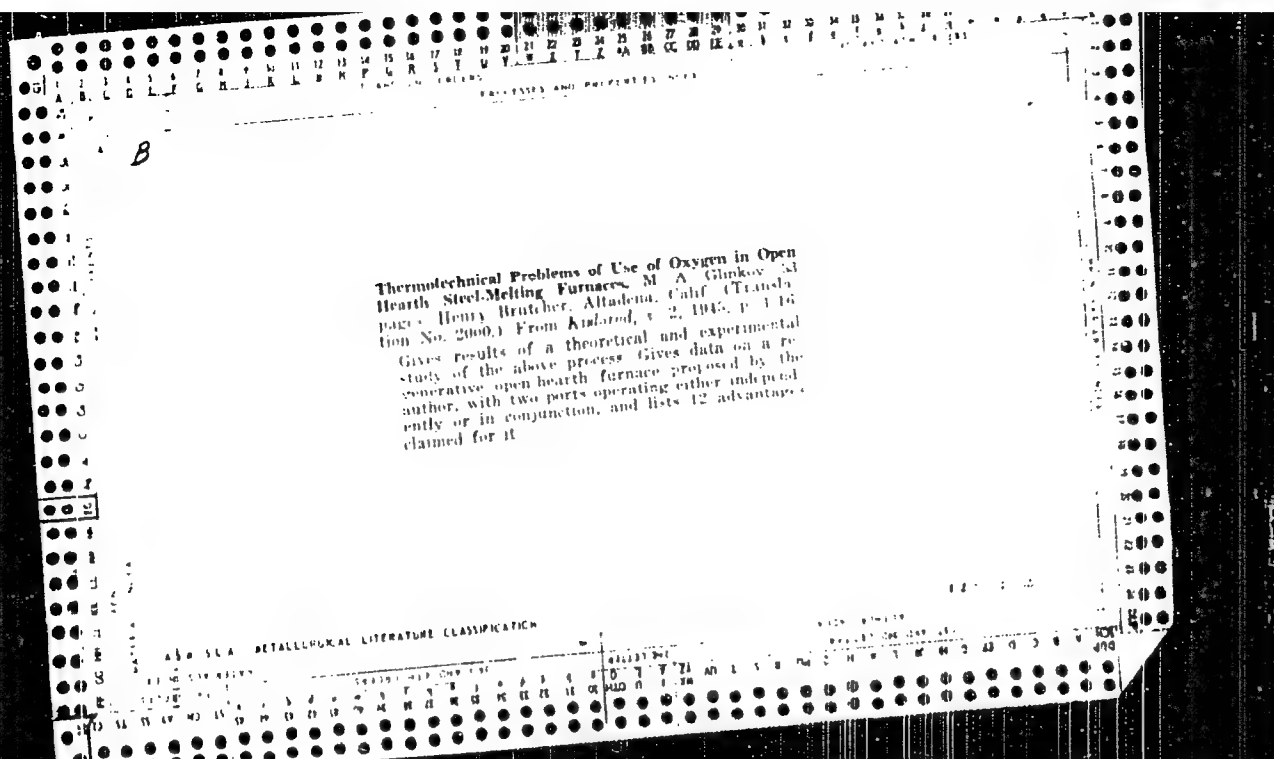
***Experimental Study of Heating Liquids (Including Molten Metals) from Above.** M. A. Glinkov (*Tekhn. Ust. Ind. Inst.*, 1911, 17, 42-51, 1-126, 1010, 40, 3655). [In Russian]. The purpose of this investigation was to test a previously stated contention that the heating of a bubbling liquid bath heated from above can be calculated by assuming a equivalent bath having a corresponding coeff. of thermal conductivity. This coeff. of thermal conductivity is referred to as the "virtual" conductivity coeff. The experiments, described in detail, were carried out with water, molten lead, and a mixture of sodium nitrate 55 and potassium nitrate 45%, at approx. 200°C. The results confirm the existence of a relation between the bubbling of a gas through a heated liquid and the rate of heating of the liquid. In the open hearth furnace, the bubbling is provided by the rising gases which result from the combustion of carbon. Up to a certain vol., the bubbling gases accelerate the rate of heating of the liquid. Beyond this point, increases in the vol. of the gas do not accelerate the rate of heating. Thus, the time required for heating an open hearth bath cannot be changed by changing the rate of burning of the carbon in it. Deepening the hearth will raise the output of metal. There is an optimum depth (not at present calculable) which gives a max. total output.

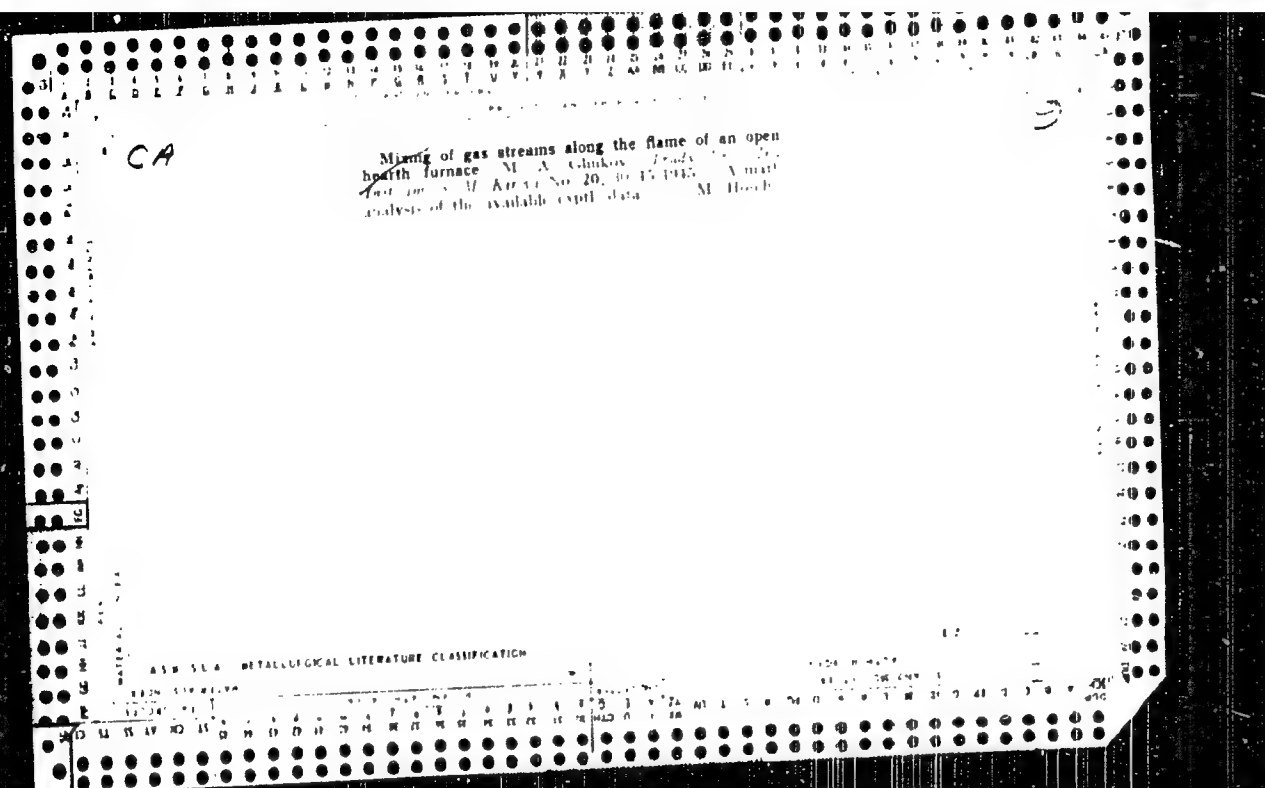


Heat exchange in the open hearth furnace

Glinkov, S. N. S. 4, 205, 11, 1944. Heat exchange in the solid charge before melting in the solid after melting begins, in the liquid bath. Heat transfer by convection from the bath and by radiation from the bath to the bath.

ASH, S. A. METALLURGICAL LITERATURE CLASSIFICATION





Heat transfer in a liquid bath agitated by bubbling
 M. A. Glinkov and V. S. Kuchin. *Dokl. Akad. Nauk SSSR*, **1966**, 1463, 72 (in Russian). Heat transfer between fused slags and metal in the open hearth process is determined by the heat cond. of the m. l. under conditions of conv. agitation by bubbling gas, mainly CO. The characteristic criterion is $G = V \rho_l \eta / 2 \pi \gamma \rho_g \mu$ (1). $G = \gamma \rho_l \eta$ eq. where $V = \text{vol. of gas per sec.}$, γ and ρ_g = specific wt. of liquid and of gas, resp., η = velocity of bubbles, ρ_l = horizontal sec. of the bath, μ = viscosity coeff. of the liquid, $H = \text{depth of bath from which the bubbles rise.}$ At a certain G , the laminar flow in the bath becomes turbulent, $G_c = 1.5 \times 10^{-3} K \rho_l \eta$, where $K = \text{Reynolds' no.}$, $K = \omega \rho_l d / \mu$, $\omega = \text{diam. of the bubbles}$. P = new criterion $\propto V \rho_l \eta$. Related to G is a "virtual" coeff. of heat cond., λ^* valid under the conditions described. $\lambda^* = C \rho_l Pr$ where $C = \text{heat capacity by wt. of the liquid}$, $Pr = \text{Prandtl's criterion}$, inversely proportional to G and to powers of $\omega \rho_l \eta$ and of $\gamma \rho_l \eta$ where $\gamma = \text{surface tension of the liquid}$. Experimentally, depend. of λ^* on V and on η was studied on an ir-bubble stirred water and wat.-glycerol mixt. bath model, with $\omega \rho_l \eta$ and $\gamma \rho_l \eta$ kept const. Under these conditions, the dimensionless plot of $\log \lambda^* / C \rho_l$ against $\log G$ is a single straight line with the exptl. points spreading around it. Numerical evaluation by the method of least squares gives $\lambda^* / C \rho_l = G^{0.4}$, that is, λ^* is basically detd. by the amt. of gas passing through a unit area of the cross section of the bath and by its depth. In turbulent flow, η of the liquid has only a minor influence; thus, practically no difference was found in λ^* on a 13 fold change of η from 65% glycerol to pure water. Industrial-scale expts. were conducted on 6 basic and acid open hearth slags in 1000-lb batches, with η measured directly and the amt. of gas derived from the rate of combustion of carbon. The equation $\lambda^* / C \rho_l = G^{0.4}$ is found to hold also for most of the slags. λ^* varies within the limits 25-92 cal./sq. cm. hr. degree.

1
CA

Intermixing of a liquid by gas bubbles. M. A. Glinkov.
Compt. rend. acad. sci. U.R.S.S. 51, 100-102 (1940). An
equation for the unit. of mixing produced by the action of
gas bubbles is developed. J. K. Taylor

ASB-51A METALLURGICAL LITERATURE CLASSIFICATION

The Question of Heat Transfer in a Molten Bath by
Bubbles. M. A. Glinkov and V. S. Kochin. (Iron and
Steel Institute, 1947, Translation Series, No. 325)
This is an English translation of a paper which appeared
in Bulletin de l'Académie des Sciences de l'U.R.S.S.,
Classe des Sciences Techniques, 1946, No. 10, pp. 1403
1472. R. A. R.

117 AND 2ND ORDERS

PROCESSES AND PROPERTIES INDEX

Analytical method for calculation of thermal conditions in the open hearth furnace. M. A. Glinkov (Sov. 1948, No. 2, 126-141, J. Iron Steel Inst., 1948, 138, 214).—A method for calculating the output of any furnace melting a standard charge without the necessity for compiling a detailed heat balance is described. Operating factors, e.g., calorific value of the fuel, nature of the flame, and the rate of charging, are allowed for. Calculations for non-standard charges are possible only if their equivalent coeff. of thermal conductivity are known. The total expenditure of heat for melting is given by an equation the terms of which include the differentials, with respect to time, of the change in temp. resulting from chemical reactions and of the heat required for heating and melting. The standard-charge concept on which the method is based involves a schematic arrangement of the CaO , ore, and metal of the charge in the furnace; the mean composition of the charge and the rate of charging are those used in practice. By making certain assumptions, operation with liquid charges can be brought into the scope of the standard-charge concept. Conventions are adopted regarding the thermal capacities of the charge and melt. The following factors are discussed on the above basis: (a) the equivalent coeff. of thermal conductivity of the charge and melt; (b) the integral coeff. of heat transfer; (c) temp. distribution in the charge and molten bath; (d) changes in heat content of the charge during heating; (e) changes in the heat content of the slag and molten metal; and (f) the equation for the heat required. As an example, the output of, and thermal conditions in, a furnace with the following characteristics are calculated: hearth area 30 sq. m.; capacity 64 tons of liquid metal; calorific value of gaseous fuel 2000 cal. per cu. m.; a product containing C 0.3, Mn 0.45 and Si trace %; a charge

118 AND 3TH ORDERS

ASB. SLA METALLURGICAL LITERATURE CLASSIFICATION

119 AND 4TH ORDERS

120 AND 5TH ORDERS

121 AND 6TH ORDERS

122 AND 7TH ORDERS

123 AND 8TH ORDERS

124 AND 9TH ORDERS

125 AND 10TH ORDERS

126 AND 11TH ORDERS

127 AND 12TH ORDERS

128 AND 13TH ORDERS

129 AND 14TH ORDERS

130 AND 15TH ORDERS

131 AND 16TH ORDERS

132 AND 17TH ORDERS

133 AND 18TH ORDERS

134 AND 19TH ORDERS

135 AND 20TH ORDERS

136 AND 21TH ORDERS

137 AND 22TH ORDERS

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141 AND 26TH ORDERS

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194 AND 79TH ORDERS

195 AND 80TH ORDERS

196 AND 81TH ORDERS

197 AND 82TH ORDERS

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199 AND 84TH ORDERS

200 AND 85TH ORDERS

201 AND 86TH ORDERS

202 AND 87TH ORDERS

203 AND 88TH ORDERS

204 AND 89TH ORDERS

205 AND 90TH ORDERS

206 AND 91TH ORDERS

207 AND 92TH ORDERS

208 AND 93TH ORDERS

209 AND 94TH ORDERS

210 AND 95TH ORDERS

211 AND 96TH ORDERS

212 AND 97TH ORDERS

213 AND 98TH ORDERS

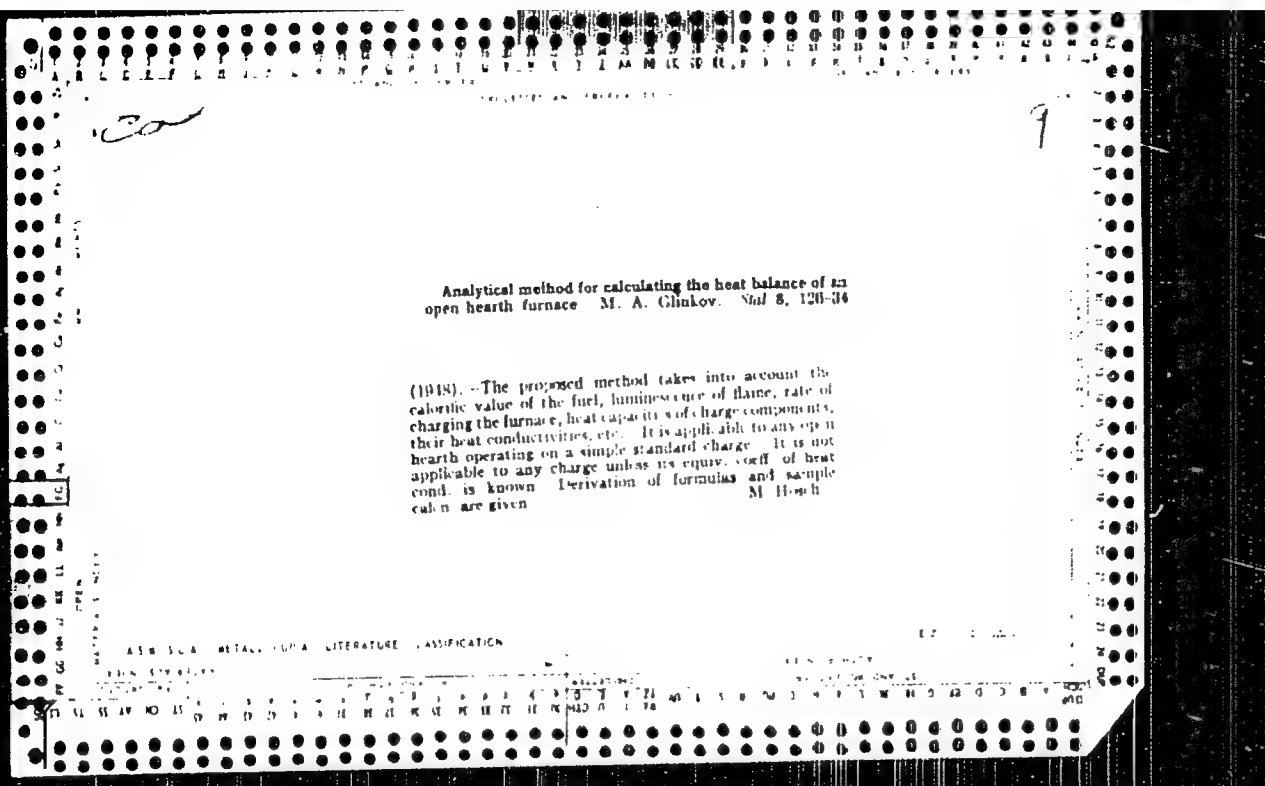
214 AND 99TH ORDERS

215 AND 100TH ORDERS

containing C 2, Mn 0-95, and Si 0-55? ; expenditure of CaO and ore
5% and 8%, respectively, of the wt. of the metallic part of the
charge.
H. B. CLARK.

11.00000000

"Comments on the Article 'Newly Published Data on the Effect of Stress' by Prof. I. I. Kitev, Israel H. I. Kitev, Soviet Union, in 'Soviet J. Geophys. Res.', No. 3, 1971, Gr. Tech. Sci. Ser., Moscow: Acad. Sci. USSR, 1971, 1-10.



GLINKOV N. A.

Glinkov, N. A. and Glinkova, O. A. INVESTIGATION OF THE RADIATION LIGHT-ABSORPTION ABILITIES (DEGREE OF BLACKNESS) OF REFRACTORY MATERIALS. Paper of the 1st. Int. Sci. Conf. Zinov, N. A., 97-116 (1969).--The light-absorption abilities of some refractory materials were studied in a series of experiments. In the first series the degree of blackness was determined by measuring the temperature of the heated specimen with a thermocouple inserted in the specimen and with a radiation pyrometer. Under these conditions the degree of blackness $\epsilon = (q^0 - q_{\text{th}}^0) / (q_{\text{th}}^0 - q_{\text{a}}^0)$, where T is the temperature determined with the radiation pyrometer, T_0 is the temperature determined with the thermocouple, and T_0 is the temperature of the pyrometer reservoir. By this method chrome-magnesite, fire clay, talc, Dinas, and magnesite brick were studied at temperatures of 700° to 1100°. For the second series a specially constructed Pt furnace was used in the pyrometer was replaced with a differential thermopile. In accordance with the denseness of their surfaces the investigated materials were divided into 6 classes. The highest emissivity was observed in the least dense materials, fireclay and improved fire clay. Cornish, andalusite, and magnesite had the least emissivity. The denseness of these materials is greater than that of the preceding materials. Dinas, ordinary magnesite, and talc brick had an emissivity between these 2 groups. For the 3rd series of experiments a furnace more like that of Veritel (of Chaleur et al., 1938, Nos. 215 and 216) was used. The temperatures investigated were 600 to 1400°. The materials investigated were fire clay, Dinas, chrome-magnesite, and magnesite. Several samples of each were taken, difference in the blackness of the specimens depending on their size composition, the larger the size the greater the degree of blackness. The differences in the degree of blackness between sizes that were 270 and 200 mesh were 4 to 50 percent for fire clay, 1 to 10; for magnesite, 12 to 17; for Dinas, 1 to 18; and for chrome-magnesite 1 to 10% less, depending on the temperature. The effect of size of the material on the degree of blackness was

(over)

671777, 778, 779.

1171 G. ...
-today. ...

Today, I have been thinking about you, and how much I love you.

$$C_1 = 2\pi \times 10^8 \times 1.5 \times 10^{-10} = 9.42 \times 10^{-2} \text{ m} = 9.42 \text{ cm}$$

Glinkov, L. A.

"Effect of the Type of Gas Flow on the Heat Transfer Processes in the Flame-Limited High Temperature Furnaces. (Vliyanie charakterov dvizheniya gaza na teploobmen v vysokotemperaturnykh pechakh s ogranichennoy zhenyem)", Glinkov and L. A. Glinkov, no. 7-111
(Structure and Properties of Steel (Struktura i svoystva stali)) in the
Government Scientific-Mechanical Publishing House of Standards and Temperature Technology,
Moscow 1961, 247 pp.)

PHASE I

TREASURE ISLAND BIBLIOGRAPHICAL REPORT

AID 601 - I

BOOK

Call No.: AF428232

Authors: GLINKOV, M. A., Dr. of Tech. Sci., Prof., et. al.

Full Title: METALLURGICAL FURNACES

Transliterated Title: Metallurgicheskiye pechi

PUBLISHING DATA

Originating Agency: None

Publishing House: State Scientific and Technical Publishing House of Literature on Ferrous and Nonferrous Metallurgy (METALLURGIZDAT)

Date: 1951 No. pp.: 975 No. of copies: 8,000

Editorial Staff: The Authors' Collective (Avtorskiy Kollektiv) with Glinkov, M. A., Dr. of Tech. Sci., Prof. as Editor-in-Chief.

Collaborating members are: Baum, V. A., Budrin, D. V.,

Vashchenko, A. I., Glinkov, M. A., Granovskiy, B. L., Kitayev, B. I.,

Kuz'min, M. A., Mikhaylenko, A. Ya., Nazarov, I. S., Plotnikov, L. A.,

Semikin, I. D., Tayts, N. Yu. and Troyb, S. G.

PURPOSE: To replace the several books used in the course at the metallurgical colleges with one comprehensive manual. Approved as a textbook by the Ministry of Higher Education of the USSR.

TEXT DATA

Coverage: Fuels and process of combustion are thoroughly analyzed.

General principles for construction of metallurgical furnaces,

various refractory and other construction materials are discussed.

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Metallurgicheskiye pechi

AID 601 - I

The basic principles of heat engineering, mechanics of gases, theory of analogies, transmission of heat, tempering, smelting and cooling of metals are treated in detail with elaborate mathematical formulae. The auxiliary equipment of the combustion chamber is minutely described and illustrated. Blast and open-hearth furnaces and the heat-treatment furnaces used in ferrous metallurgy, the shaft furnaces, reverberatory, tubular rotary and crucible furnaces used in nonferrous metallurgy, as well as electric resistance, induction and electric arc furnaces are described. (Electric furnaces in ferrous metallurgy and their control and automatic equipment are not given but will be discussed in a book to be published later). The book is abundantly illustrated with diagrams, mathematical formulae and charts. This book is compiled by collaboration. The 13 authors presented a chapter or division. Their manuscripts underwent a mutual evaluation, correction and critical discussion by the other members of the collective, and then were incorporated into the book.

No. of References: 175 Russian, 1925-1950

Facilities: Moskva Institute of Steel; Ural Polytechnic Institute; Dnepropetrovsk Metallurgical Institute; Moskva Institute of Nonferrous Metals and Gold; Leningrad Polytechnic Institute; Siberian Metallurgical Institute; and State Scientific Research Institute of Nonferrous Metals.

2/2

GIENNY, L. A. (1957) - LADON, L. A. (1957); LADON, L. A. (1957).

"General Principles of Polymer Testing," in: Handbook of Polymer Testing
(Metallurgical Engineering, 1957), 1-11.

GUINOV, M. A. (P. 5.) CHEN, Y. A. (P. 1.)

"The Relevance of China" From the Chinese to the United States (Notes) Prin-
ced, by the U.S. State Dept. 1951.

GLINKOV M.A

3

USSR

✓ Influence of the pattern of gas travel on heat-exchange processes in high-temperature flame furnaces. M. A. Glinkov and G. M. Kapustin. *Soviet Eng. Tech. J.* 1951, 35, 111. (1951).—An extensive study of the heating mechanism in a 10-ton exptl. open-hearth furnace fired with a natural gas burner, the inclination of which to the bath was changed from 10 to 40°. A greater inclination of the flame widens the flame and spreads it in the direction perp. to the axis of the burner until it strikes the surface of the bath. After this the action of the flame becomes U-shaped and has a greater thermal efficiency. Temp. distribution obtained with different positions of the burner is given in diagram. 18 references. I. G. G.

A B

D

A S M

264-D. The Construction of Uniflow
Steel Melting Furnaces. (In Russian)
M. A. Glinkov. Za Ekonomicheskoye
Soyuz. Feb. 1982, p. 25-27.
The uniflow process in open
hearth furnaces as a means of in-
creasing production and simplifying
operation. (P2 ST)

G. L. NIKOV, M. A.

Problems of Metallurgy, Academy of Sciences of the
U.S.S.R., Moscow, 1963. Electrochemical Investigations in
the Field of Ferrometallurgy, O. A. Belyi (64-12) [In
Russian]. Work on a number of high-temperature galvanic
cells with fused salts as the electrolyte is described. These
have been studied electrochemically and in galvanic cells with
an iron electrode. Electrodepositional effects have also been
studied. The kinetics of metal/slag reactions are discussed.
Influence of Dissolving Elements on the Activity of Oxygen
Dissolved in Liquid Iron & Manganese. (70-88). Equilibria
between oxygen in liquid iron and silicon, vanadium, and
other deoxidizing elements are considered, and the influence
of these elements on the activity of oxygen is discussed.

144E2C

GLINKOV, M.A., professor, doktor; REKHTMAN, M.Ya., kandidat tekhnicheskikh nauk.
~~Metallurgicheskiye pechi~~

Movement of gases in the hearth of open-hearth furnaces. Sbor.Inst.stali
no.31:285-317 '53. (MIRA 9:9)

1.Kafedra "Metallurgicheskiye pechi".
(Open-hearth furnaces) (Gas flow)

USSR.

✓ A "fire-stand" investigation of heat exchange inside the furnace. M. A. Glinkov and A. G. Zen'kovskii. Izv. Akad. Nauk S.S.S.R., Otdel. Tekh. Nauk 1954, No. 11, 108-23. The term "fire-stand" was coined to represent an app. for measuring heat exchange; the metal to be heated is replaced by a heat-absorbing and measuring device, which, on the heat-absorption side is provided with additional heat resistance in the form of thin plates of fire-proof material with a degree of blackness equal to the blackness of the replaced metal. The proposed method permits the study of heat processes inside a fire furnace on a small geometrical model. W. M. Skatnikov

GLINKO, M. A.

1340* Heat Exchange in Continuous Furnaces. O teploob-
mene v metodicheskikh perhakh. (Russian.) M. A. Glinko
and A. G. Zerkovskii. Izvestia akademii nauk SSSR
tekhnicheskikh nauk, 1955, no. 10, Oct., p. 138-143.
Effect of screen on heat-exchange intensity; efficiency of direct-
flow continuous two-zone furnaces; comparison of variations of
counter- and direct-flow arrangements; calculations of radiant
heat exchange. Diagrams, graphs. 2 ref.

ML
92
①

GLINKOV, M.A.; VAVILOV, N.S.

Instruments for investigating the thermal operation of metallurgical
furnaces. Zav.lab.21 no.10:1203-1207 '55. (MLRA 9:1)

1.Moskovskiy institut stali imeni Stalina.
(Thermometers) (Metallurgical furnaces)

"APPROVED FOR RELEASE: 09/24/2001

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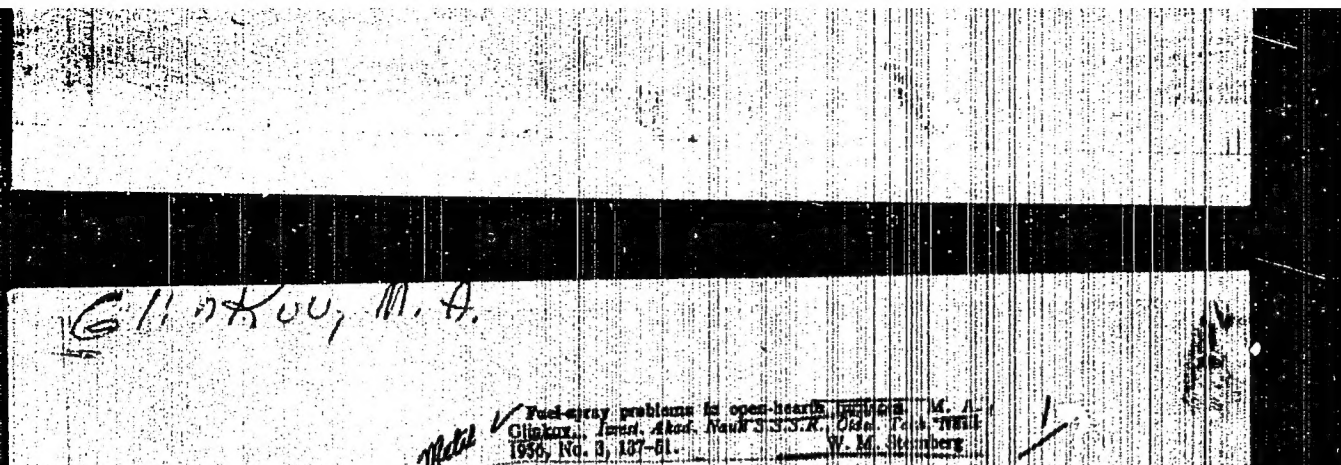
Glinkov, M.A.

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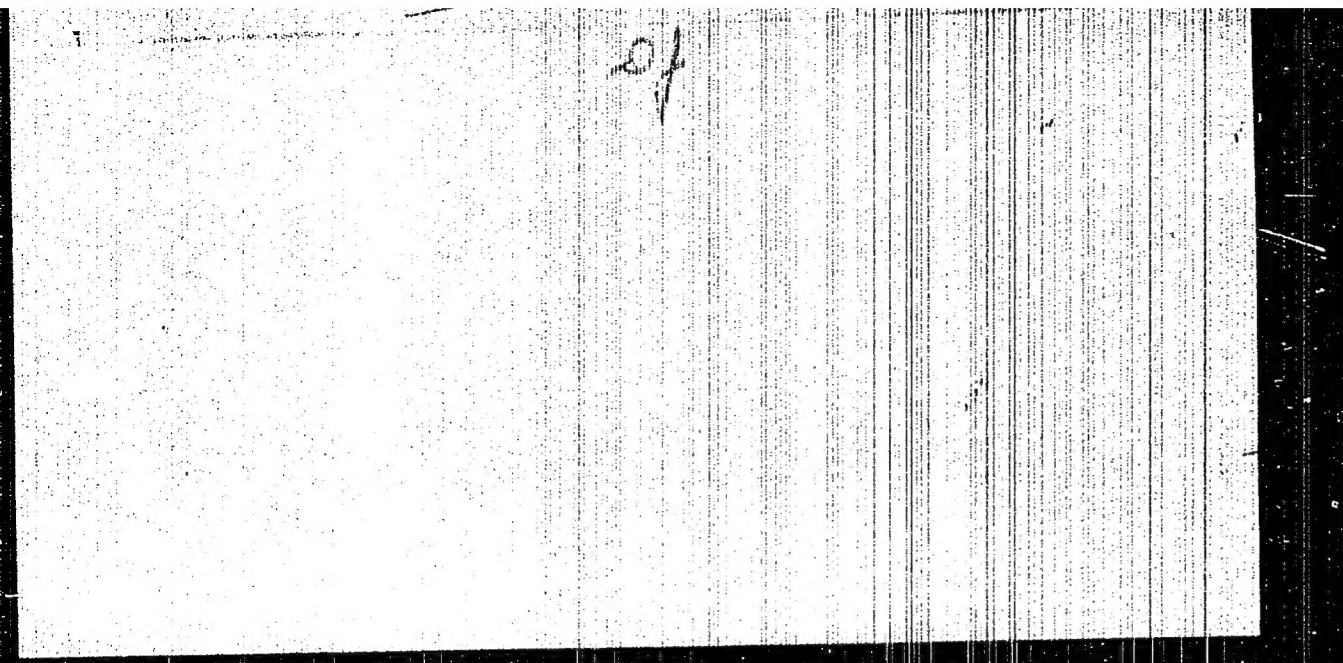
✓ 998. DEVICES FOR INVESTIGATING THE THERMAL WORK OF METALLURGICAL
FURNACES. Glikov, N.A. and Pavlov, N.S. (Zavod. Lab. (Fact. Lab.,
Moscow, 1959, Vol. 27, No. 1203-1207). Some newer calorimeters (70 cal heat
flow meters) are critically considered, with special reference to their use in
steel-making furnaces. Details are given of instruments developed at the
Moscow Steel Institute.

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